Observations and Analysis of the Extreme Mass Ratio, High Fill-out Solar Type Binary, V1695 Aquilae

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Abstract CCD BVR $_{0.6}$ light curves of V1695 Aquilae were taken during the Fall 2016 season at the Cerro Tololo InterAmerican Observatory with the 0.6-meter reflector of the SARA South observatory in remote mode. It is an eclipsing binary with a period of 0.41283 d. The light curves yield a total eclipse (duration: 59 minutes) but have an amplitude of only ~0.4 mag. The spectral type is ~G8V (~5500 K). Four times of minimum light were calculated, all primary eclipses, from our present observations. We calculated linear and quadratic ephemerides from all available times of minimum light. A 17-year period study reveals a quadratic orbital period decrease at a high level of confidence. The orbital period is changing at a rapid rate of of dp/dt= -1.73×10^{-6} d/yr. The solution is that of an Extreme Mass Ratio Binary. The mass ratio is found to be near 0.16. Its Roche Lobe fill-out is a hefty 83%. The small component has the slightly hotter temperature of ~5650 K, which makes it a W-type W UMa Binary. As expected in binaries of this spectral type, it has cool spot regions.

1. Introduction

In this study of V1695 Aql, our analysis includes its observation, a period study, and light curve analysis of an extreme mass ratio solar type Southern eclipsing binary. We used the Wilson-Devinney Program (wD; Wilson and Devinney 1971) for this calculation. This paper represents the first published BVRcIc light curves and analysis of V1695 Aql. Observers prize total eclipsing contact binaries since they give unambiguous solutions with mass ratios even without difficultto-obtain precision radial velocity curves. These require large telescopes (we estimate a 3.5 to 4-meter telescope is needed for this variable). Many forget about velocity smearing with such a system which requires a higher signal-to-noise.

Contact binaries are numerous in number and represent a challenge to present-day stellar theory. It is believed that (for those of solar type), that they begin their existence as well detached fast spinning stars in groups that undergo gravitational interactions which leave them as binaries with several-day periods. Since they are highly magnetic in nature, due to their convective envelopes and fast rotation, they undergo magnetic braking as plasma winds leave the stars on stiff rotating dipole fields. This action torques the binary, eventually bringing them into contact and finally leaving a single, fast rotating star.

2. History and observations

V1695 Aql (GSC 5149 2845) was discovered as part of an initiative to classify variable stars using CCD observations by Bernhard *et al.* (2002). The star was typed as a W UMa binary with a V magnitude \approx 11.0. Their light curve is shown as Figure 1.

Their ephemeris is:

 $MinI = HJD \ 2452522.440 \pm 0.007 + 0.4128 \pm 0.0001 \ d \times E \ (1)$



Figure 1. Light curve of V1695 Aql by Bernhard et al. 2002.

Kreiner (2004) gives the following:

$$MinI = HJD \ 2456102.460 + 0.4127768 \ d \times E$$
(2)

A number of eclipse timings are given by Pejcha (2005), Berhard *et al.* (2002), and Paschke (1994, 2002).

V1695 Aql is likely an x-ray source (1RXSJ193821.2-033245), which is not unusual for active W UMa variables (Szczygiel *et al.* 2008). It is included in the Automated Variable Star classification (ID 14143847) via the NSVS (Hoffman *et al.* 2009) and is listed in the 78th name list (Kazarovets *et al.* 2006). The observations were undertaken by Samec, Gray, Faulkner, Hill, and Van Hamme. Reduction and analyses were done by Samec and Gray.

3. Photometry

Our photometry was taken with the Southeastern Association for Research in Astronomy (SARA South) Telescope at Cerro Tololo InterAmerican Observatory (CTIO) in remote mode. The 24-inch f/11 Boller and Chivens reflector was used on four nights, 14 August and 3-5 September, 2016, with the ARC Camera cooled to -60° C. We used standard BVR I Johnson-Cousins filters. The precision of a single observation was good, 0.010 in B, V, I, and 0.014 in R. The observations included 185 in B, 187 in V, 162 in R, and 187 in I. Exposure times varied from 250-275 seconds in B, 80-90 seconds in V, and 30–50 seconds in R_a and I_a. Nightly images were calibrated with 25 bias frames, at least five flat frames in each filter, and ten 300-second dark frames. Figure 2a and 2b show sample observations of B, V, and B-V color curves on the night of August 14 and September 23, 2016. Our observations are given in Table 1, in delta magnitudes, ΔB , ΔV , ΔR_{a} , and ΔI_{a} , in the sense of variable minus comparison star.

4. Finding chart

The finding chart is shown as Figure 3. The coordinates and magnitudes of the variable star, comparison star, and check star are given in Table 2. Our B–V and R_c–I_c Comparison-Variable magnitude curves show that the variable and comparison stars are near spectral matches with Δ (B–V) and Δ (R–I) \approx 0. The nightly C–K values stayed constant throughout the observing run with a precision of \approx 1%.

5. Period study

Four times of minimum light were calculated from our present observations, all primary eclipses, using the method of Kwee and Van Woerden (1956) performed by Caton:

$$HJD = 2457614.68359 \pm 0.0002 d$$

2457634.49320 \pm 0.00037 d
2457636.56250 \pm 0.00006 d
2457635.68247 \pm 0.00002 d

Additional timings were gathered from other sources using the O–C gateway (http://var2.astro.cz/ocgate/) and the Nelson

Database of Times of Minima (Nelson 2016). These included Berhard *et al.* (2002), and Pejcha (2005). We note that our last timing was removed from our analysis due to its large residual. The following linear and quadratic ephemerides were determined from all available times of minimum light:

JD Hel MinI =
$$2452576.3106 \pm 0.0060 d$$

+ $0.41282964 \pm 0.00000080 \times E$ (2)

JD Hel MinI =
$$2452576.3191 \pm 0.0024 d$$

+ $0.4128401 \pm 0.0000011 \times E -9.75 \pm 1.0 \times 10^{-10} \times E^2$ (3)

The O–C residuals for both linear and quadratic calculations are given in Table 3. Thus, the 17-year period study reveals that the system is undergoing a smooth quadratic decrease in orbital period. The changing period would be expected for the process of magnetic braking (e.g., Gazeas and Stępień 2008). The value of the rate of change in the orbital period is $dp/dt = -1.73 \times 10^{-6} d/yr$. Third body interactions and normal stellar evolution may play a role, but a much longer interval of observation is needed to determine if this is the case. A plot of the quadratic term overlying the linear residuals of Equation 3 is shown in Figure 4.

6. Light curve characteristics

The light curves of V1695 Aql phased using Equation 2, delta mag vs. phase, are shown in Figure 5a and 5b. Light curve amplitudes and the differences in magnitudes at various quadratures are given in Table 4. The primary amplitudes of the light curves are about 0.4 magnitude in all filters while the secondary's are ~ 0.3 magnitude. This points to a rather large difference in minima, 0.07-0.08 magnitude, for an over contact binary. These values are usually thought of as indicators of the degree of thermal contact. In this case, it may be an indicator of large spot regions. In general, the asymmetries throughout the light curve point to the presence of spot activity. This is apparent when we compare the early curve (Figure 1) to our present ones. In Figure 6, a plot of the night to night variability in the light curves in B and V is given. This shows that the magnetic activity causes rapid changes in the light curves. The light curves are distinctly over contact. The low amplitudes indicate that the binary has a very small mass ratio so the binary belongs to the family of extreme-mass ratio binaries. To extend this analysis we undertook a Wilson-Devinney program light curve solution. The light curves yielded a very long eclipse duration of 59 minutes for a binary, with a period of 9.9 hours as determined from this solution.

7. Temperature and light curve solution

BINARY MAKER 3.0 (Bradstreet and Steelman 2002) was used to explore the character of our light curves and determine initial parameters of each of the B, V, Rc, Ic light curves. The Wilson-Deviney program requires a fairly good fitting curve to begin the process, however the final solution parameters may have little resemblance to the initial values. For instance, our B-filter light curve gave a mass-ratio of 0.15 using BINARY



Figure 2a. B, V, and B–V color curves of V1695 Aql on the night of August 14, 2016.



Figure 2b. B, V, and B–V color curves of V1695 Aql on the night of September 23, 2016.



Figure 3. Finding Chart of V1695 Aql including Variable (V), Comparison (C), and Check Stars (K).



Figure 4. O–C residuals from the quadratic ephemeris of V1695 Aql from Equation 3.



Figure 5a. B, V delta magnitudes of V1695 Aql, phased using Equation 2.



Figure 5b. R., I. delta magnitudes of V1695 Aql, phased using Equation 2.

Table 1. V1695 Aql observations, ΔB , ΔV , ΔR_c , and ΔI_c , variable star minus comparison star.

ΔB	HJD 2457600+	ΔB	HJD 2457600+	ΔB	HJD 2457600+	ΔB	HJD 2457600+	ΔB	HJD 2457600+
-1.042	14.4856	-1.093	14.6709	-1.258	34.538	-1.415	35.604	-1.138	36.549
-1.044	14.4903	-1.089	14.676	-1.297	34.543	-1.418	35.609	-1.137	36.554
-1.054	14.4954	-1.090	14.682	-1.347	34.548	-1.432	35.615	-1.121	36.560
-1.079	14.5006	-1.096	14.687	-1.365	34.553	-1.435	35.620	-1.123	36.565
-1.108	14.5058	-1.091	14.693	-1.381	34.559	-1.445	35.625	-1.123	36.571
-1.144	14.5111	-1.100	14.698	-1.404	34.564	-1.446	35.630	-1.145	36.576
-1.100 -1.218	14.5105	-1.112	14.704	-1.403 -1.424	34.309	-1.433	35.635	-1.143	36.587
-1.250	14.5268	-1.177	14.718	-1.441	34.579	-1.424	35.646	-1.187	36.593
-1.312	14.5373	-1.214	14.724	-1.438	34.585	-1.427	35.651	-1.226	36.598
-1.337	14.5425	-1.241	14.729	-1.256	35.483	-1.410	35.656	-1.269	36.604
-1.369	14.5500	-1.270	14.735	-1.228	35.488	-1.391	35.661	-1.294	36.609
-1.376	14.5554	-1.302	14.740	-1.184	35.494	-1.388	35.667	-1.322	36.614
-1.375	14.5609	-1.319	14.746	-1.158	35.499	-1.377	35.672	-1.339	36.620
-1.401	14.5663	-1.338	14.751	-1.107	35.505	-1.345	35.678	-1.367	36.625
-1.398	14.5/18	-1.35/	14.757	-1.080	35.510	-1.310	35.684	-1.382	36.631
-1.407 -1.404	14.3773	-1.374 -1.392	14.705	-1.074	35.515	-1.292	36.461	-1.400	36.642
-1.400	14.5882	-1.404	14.774	-1.068	35.526	-1.399	36.466	-1.416	36.647
-1.396	14.5937	-1.168	34.465	-1.060	35.531	-1.404	36.473	-1.425	36.653
-1.382	14.5992	-1.137	34.469	-1.067	35.537	-1.418	36.478	-1.427	36.658
-1.372	14.6052	-1.123	34.475	-1.079	35.542	-1.397	36.483	-1.435	36.664
-1.358	14.6107	-1.137	34.480	-1.085	35.547	-1.379	36.489	-1.443	36.669
-1.338	14.6162	-1.137	34.486	-1.098	35.552	-1.365	36.494	-1.432	36.675
-1.314	14.6216	-1.138	34.491	-1.132	35.557	-1.351	36.500	-1.432	36.680
-1.296	14.62/1	-1.127	34.496	-1.1/0	35.563	-1.338	36.505	-1.433	36.686
-1.278 -1.248	14.0320	-1.140 -1.145	34.501	-1.207 -1.262	35.508	-1.308 -1.281	36.510	-1.397	36.094
-1.240 -1.207	14.6331	-1.145	34 512	-1.202	35 578	-1 259	36 521	-1.357	36 705
-1.177	14.6490	-1.154	34.517	-1.315	35.583	-1.221	36.527	-1.335	36.711
-1.129	14.6545	-1.188	34.522	-1.350	35.588	-1.187	36.532		
-1.103	14.6600	-1.211	34.527	-1.363	35.594	-1.161	36.538		
-1.103 -1.096	14.6600 14.6654	-1.211 -1.228	34.527 34.533	-1.363 -1.385	35.594 35.599	$-1.161 \\ -1.150$	36.538 36.543		
-1.103 -1.096 ΔV	14.6600 14.6654 <i>HJD</i> 2457600+	-1.211 -1.228	34.527 34.533 <i>HJD</i> 2457600+	$\begin{array}{c c} -1.363 \\ -1.385 \end{array}$	35.594 35.599 <i>HJD</i> 2457600+	-1.161 -1.150 ΔV	36.538 36.543 <i>HJD</i> 2457600+		HJD 2457600+
-1.103 -1.096 ΔV -1.088	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493	-1.211 -1.228 ΔV -1.284	34.527 34.533 <i>HJD</i> 2457600+ 14.634	$ -1.363 \\ -1.385 \\ \Delta V \\ -1.418 \\ $	35.594 35.599 <i>HJD</i> 2457600+ 14.781	-1.161 -1.150 ΔV -1.423	36.538 36.543 <i>HJD</i> 2457600+ 34.590	Δ <i>V</i>	<i>HJD</i> 2457600+ 35.677
-1.103 -1.096 ΔV -1.088 -1.084	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	34.527 34.533 <i>HJD</i> 2457600+ 14.634 14.640	$\begin{array}{c c} -1.363 \\ -1.385 \\ \hline \\ \Delta V \\ \hline \\ -1.418 \\ -1.407 \end{array}$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779	$\begin{array}{c c} -1.161 \\ -1.150 \\ \hline \\ \Delta V \\ -1.423 \\ -1.443 \end{array}$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595	Δ <i>V</i> -1.337 -1.319	<i>HJD</i> 2457600+ 35.677 36.511
-1.103 -1.096 ΔV -1.088 -1.084 -1.110	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497 14.502	$\begin{array}{ c c c c c } -1.211 \\ -1.228 \\ \hline & \Delta V \\ \hline & -1.284 \\ -1.249 \\ -1.226 \\$	34.527 34.533 <i>HJD</i> 2457600+ 14.634 14.640 14.645	$\begin{vmatrix} -1.363 \\ -1.385 \end{vmatrix}$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785	$\begin{array}{ c c c c c } -1.161 \\ -1.150 \\ \hline \\ & \Delta V \\ \hline \\ -1.423 \\ -1.443 \\ -1.057 \\ \hline \\ -1.057 \\ \hline \end{array}$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546	Δ <i>V</i> -1.337 -1.319 -1.280	<i>HJD</i> 2457600+ 35.677 36.511 36.516
-1.103 -1.096 ΔV -1.088 -1.084 -1.110 -1.139 1.100	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497 14.502 14.507 14.512	$\begin{array}{ c c c c c } -1.211 \\ -1.228 \\ \hline & \Delta V \\ \hline & -1.284 \\ -1.249 \\ -1.226 \\ -1.180 \\ -1.180 \\ -1.181 \\ \end{array}$	34.527 34.533 <i>HJD</i> 2457600+ 14.634 14.640 14.645 14.651 14.651	$\begin{vmatrix} -1.363 \\ -1.385 \end{vmatrix}$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 24.470	$\begin{array}{ c c c c c } -1.161 \\ -1.150 \\ \hline \\ & \Delta V \\ \hline \\ -1.423 \\ -1.443 \\ -1.057 \\ -1.074 \\ -1.074 \\ 102 \end{array}$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 25.557	Δ <i>V</i> -1.337 -1.319 -1.280 -1.262	<i>HJD</i> 2457600+ 35.677 36.511 36.516 36.522 26.527
$\begin{array}{c} -1.103 \\ -1.096 \end{array}$	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497 14.502 14.507 14.513 14.518	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	34.527 34.533 <i>HJD</i> 2457600+ 14.634 14.640 14.645 14.651 14.656 14.656 14.652	$\begin{vmatrix} -1.363 \\ -1.385 \end{vmatrix}$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 24.481	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 25.562	ΔV -1.337 -1.319 -1.280 -1.262 -1.226 -1.226	<i>HJD</i> 2457600+ 35.677 36.511 36.516 36.522 36.527 26.533
$\begin{array}{c} -1.103 \\ -1.096 \end{array}$	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497 14.502 14.507 14.513 14.513 14.518 14.523	$\begin{array}{ c c c c c }\hline -1.211 \\ -1.228 \\ \hline & & \\ \hline & & \\ \hline & & \\ \hline & & \\ -1.284 \\ -1.249 \\ -1.226 \\ -1.180 \\ -1.180 \\ -1.141 \\ -1.120 \\ -1.109 \\ \end{array}$	34.527 34.533 <i>HJD</i> 2457600+ 14.634 14.640 14.645 14.651 14.656 14.656 14.662 14.667	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.470 34.476 34.481 34.481	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.572	ΔV -1.337 -1.319 -1.280 -1.262 -1.226 -1.175 -1.145	HJD 2457600+ 35.677 36.511 36.516 36.522 36.527 36.533 36.533
$\begin{array}{c} -1.103 \\ -1.096 \end{array}$	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497 14.502 14.507 14.513 14.518 14.523 14.528	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	34.527 34.533 <i>HJD</i> 2457600+ 14.634 14.640 14.645 14.651 14.656 14.662 14.667 14.673	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 34.476 34.481 34.487 34.482	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.572 35.572	ΔV -1.337 -1.319 -1.280 -1.262 -1.226 -1.145 -1.145	HJD 2457600+ 35.677 36.511 36.516 36.522 36.527 36.533 36.538 36.538
$\begin{array}{c} -1.103 \\ -1.096 \end{array}$	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497 14.502 14.507 14.513 14.518 14.523 14.528 14.528 14.534	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	34.527 34.533 <i>HJD</i> 2457600+ 14.634 14.640 14.645 14.651 14.656 14.662 14.667 14.673 14.678	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 34.481 34.481 34.487 34.492 34.497	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.572 35.572 35.577 35.582	ΔV -1.337 -1.319 -1.280 -1.262 -1.226 -1.175 -1.145 -1.146 -1.133	<i>HJD</i> 2457600+ 35.677 36.511 36.516 36.522 36.527 36.533 36.538 36.544 36.549
$\begin{array}{c} -1.103 \\ -1.096 \\ \hline \\ \Delta V \\ \hline \\ -1.088 \\ -1.084 \\ -1.110 \\ -1.139 \\ -1.180 \\ -1.207 \\ -1.243 \\ -1.267 \\ -1.304 \\ -1.325 \\ \end{array}$	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497 14.502 14.502 14.507 14.513 14.518 14.523 14.528 14.528 14.534 14.539	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	34.527 34.533 <i>HJD</i> 2457600+ 14.634 14.640 14.645 14.651 14.656 14.662 14.667 14.673 14.678 14.683	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 34.481 34.487 34.492 34.497 34.502	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.572 35.572 35.577 35.582 35.588	ΔV -1.337 -1.319 -1.280 -1.262 -1.226 -1.175 -1.145 -1.145 -1.146 -1.133 -1.131	<i>HJD</i> 2457600+ 35.677 36.511 36.516 36.522 36.527 36.533 36.538 36.544 36.549 36.555
$\begin{array}{c} -1.103 \\ -1.096 \\ \hline \\ -1.088 \\ -1.084 \\ -1.110 \\ -1.139 \\ -1.180 \\ -1.207 \\ -1.243 \\ -1.267 \\ -1.304 \\ -1.325 \\ -1.341 \\ \end{array}$	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497 14.502 14.507 14.513 14.518 14.523 14.528 14.528 14.534 14.539 14.546	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	34.527 34.533 <i>HJD</i> 2457600+ 14.634 14.640 14.645 14.651 14.656 14.662 14.667 14.673 14.678 14.683 14.683 14.689	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 34.481 34.487 34.492 34.497 34.502 34.507	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.572 35.572 35.577 35.582 35.588 35.593	$\begin{tabular}{ c c c c c c } \hline & \Delta V \\ \hline & -1.337 \\ -1.319 \\ -1.280 \\ -1.262 \\ -1.226 \\ -1.175 \\ -1.145 \\ -1.145 \\ -1.146 \\ -1.133 \\ -1.131 \\ -1.138 \end{tabular}$	<i>HJD</i> 2457600+ 35.677 36.511 36.516 36.522 36.527 36.533 36.538 36.544 36.549 36.555 36.560
$\begin{array}{c} -1.103 \\ -1.096 \\ \hline \\ -1.088 \\ -1.084 \\ -1.100 \\ -1.139 \\ -1.180 \\ -1.207 \\ -1.243 \\ -1.267 \\ -1.304 \\ -1.325 \\ -1.341 \\ -1.368 \\ \hline \\ -1.368 \\ -1.36$	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497 14.502 14.507 14.513 14.518 14.523 14.528 14.528 14.528 14.534 14.539 14.546 14.552	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	34.527 34.533 <i>HJD</i> 2457600+ 14.634 14.640 14.645 14.651 14.656 14.662 14.667 14.673 14.678 14.683 14.689 14.694 14.694	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 34.481 34.487 34.492 34.497 34.502 34.507 34.512	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.572 35.572 35.572 35.572 35.582 35.588 35.593 35.593	$\begin{tabular}{ c c c c c c c } & \Delta V \\ & -1.337 \\ & -1.319 \\ & -1.280 \\ & -1.262 \\ & -1.226 \\ & -1.175 \\ & -1.145 \\ & -1.145 \\ & -1.146 \\ & -1.133 \\ & -1.131 \\ & -1.138 \\ & -1.129 \\ \hline \end{tabular}$	HJD 2457600+ 35.677 36.511 36.516 36.522 36.527 36.533 36.538 36.544 36.549 36.555 36.560 36.566
$\begin{array}{c} -1.103 \\ -1.096 \end{array}$	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497 14.502 14.507 14.513 14.518 14.523 14.528 14.528 14.534 14.534 14.539 14.546 14.552 14.557 14.557	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	34.527 34.533 <i>HJD</i> 2457600+ 14.634 14.640 14.645 14.651 14.656 14.662 14.667 14.673 14.678 14.683 14.683 14.689 14.694 14.700	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 34.481 34.487 34.492 34.497 34.502 34.507 34.512 34.517 24.523	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.572 35.572 35.572 35.572 35.582 35.588 35.593 35.598 35.603 25.603	ΔV -1.337 -1.319 -1.280 -1.262 -1.226 -1.175 -1.145 -1.146 -1.133 -1.131 -1.138 -1.129 -1.124	HJD 2457600+ 35.677 36.511 36.516 36.522 36.527 36.533 36.538 36.544 36.549 36.555 36.560 36.566 36.571 26.577
$\begin{array}{c} -1.103 \\ -1.096 \end{array}$	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497 14.502 14.507 14.513 14.518 14.523 14.528 14.528 14.534 14.534 14.539 14.546 14.552 14.557 14.562 14.562	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	34.527 34.533 <i>HJD</i> 2457600+ 14.634 14.640 14.645 14.651 14.656 14.662 14.667 14.673 14.678 14.678 14.683 14.683 14.689 14.694 14.700 14.705	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 34.481 34.487 34.492 34.497 34.502 34.507 34.512 34.517 34.523 32,528	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.572 35.572 35.572 35.577 35.582 35.578 35.588 35.593 35.598 35.603 35.608 25.614	$\begin{tabular}{ c c c c c c c } & \Delta V & \\ & -1.337 & \\ & -1.319 & \\ & -1.280 & \\ & -1.262 & \\ & -1.226 & \\ & -1.175 & \\ & -1.145 & \\ & -1.145 & \\ & -1.145 & \\ & -1.146 & \\ & -1.133 & \\ & -1.131 & \\ & -1.138 & \\ & -1.129 & \\ & -1.124 & \\ & -1.140 & \\ & 1.132 & \\ \end{tabular}$	HJD 2457600+ 35.677 36.511 36.516 36.522 36.527 36.533 36.538 36.544 36.549 36.555 36.560 36.566 36.571 36.577 26.582
$\begin{array}{c} -1.103 \\ -1.096 \\ \hline \\ \Delta V \\ \hline \\ -1.088 \\ -1.084 \\ -1.110 \\ -1.139 \\ -1.180 \\ -1.207 \\ -1.243 \\ -1.267 \\ -1.304 \\ -1.325 \\ -1.304 \\ -1.326 \\ -1.368 \\ -1.369 \\ -1.394 \\ -1.404 \\ -1.410 \\ \end{array}$	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497 14.502 14.507 14.513 14.518 14.523 14.528 14.528 14.534 14.539 14.546 14.552 14.557 14.562 14.568 14.573	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	34.527 34.533 <i>HJD</i> 2457600+ 14.634 14.640 14.645 14.651 14.656 14.662 14.667 14.673 14.678 14.673 14.678 14.683 14.689 14.694 14.700 14.705 14.714 14.720	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 34.481 34.487 34.492 34.492 34.497 34.502 34.507 34.512 34.517 34.523 34.523 34.528 34.533	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.572 35.572 35.572 35.572 35.577 35.582 35.588 35.593 35.598 35.603 35.608 35.614 35.619	ΔV -1.337 -1.319 -1.280 -1.262 -1.226 -1.175 -1.145 -1.145 -1.146 -1.133 -1.131 -1.138 -1.129 -1.124 -1.140 -1.133 -1.145	HJD 2457600+ 35.677 36.511 36.516 36.522 36.527 36.533 36.538 36.544 36.549 36.555 36.560 36.566 36.571 36.577 36.582 36.582
$\begin{array}{c} -1.103 \\ -1.096 \\ \hline \\ \Delta V \\ \hline \\ -1.088 \\ -1.084 \\ -1.110 \\ -1.139 \\ -1.180 \\ -1.207 \\ -1.243 \\ -1.267 \\ -1.304 \\ -1.325 \\ -1.341 \\ -1.368 \\ -1.369 \\ -1.394 \\ -1.410 \\ -1.410 \\ -1.408 \\ \end{array}$	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497 14.502 14.507 14.513 14.518 14.523 14.523 14.528 14.534 14.534 14.552 14.557 14.562 14.568 14.573 14.579	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	34.527 34.533 <i>HJD</i> 2457600+ 14.634 14.640 14.645 14.651 14.656 14.662 14.667 14.673 14.678 14.678 14.683 14.683 14.694 14.700 14.705 14.714 14.720 14.725	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 34.476 34.481 34.487 34.492 34.492 34.497 34.502 34.507 34.512 34.517 34.512 34.517 34.523 34.528 34.533 34.538	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.572 35.572 35.572 35.577 35.582 35.578 35.598 35.598 35.603 35.603 35.608 35.614 35.619 35.624	ΔV -1.337 -1.319 -1.280 -1.262 -1.226 -1.175 -1.145 -1.146 -1.133 -1.131 -1.138 -1.129 -1.124 -1.140 -1.133 -1.145 -1.145	HJD 2457600+ 35.677 36.511 36.516 36.522 36.527 36.533 36.538 36.544 36.549 36.555 36.560 36.560 36.566 36.571 36.577 36.582 36.588 36.588 36.593
$\begin{array}{c} -1.103 \\ -1.096 \\ \hline \\ \Delta V \\ \hline \\ \hline \\ -1.088 \\ -1.084 \\ -1.110 \\ -1.139 \\ -1.180 \\ -1.207 \\ -1.243 \\ -1.267 \\ -1.304 \\ -1.325 \\ -1.341 \\ -1.368 \\ -1.368 \\ -1.369 \\ -1.394 \\ -1.404 \\ -1.410 \\ -1.408 \\ -1.415 \\ \end{array}$	14.6600 14.6654 <i>HJD</i> 2457600+ 14.493 14.497 14.502 14.507 14.513 14.513 14.518 14.523 14.528 14.528 14.534 14.539 14.546 14.552 14.557 14.562 14.568 14.573 14.579 14.584	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{r} 34.527\\ 34.533\\ \hline \\ HJD\\ 2457600+\\ \hline \\ 14.634\\ 14.640\\ 14.645\\ 14.651\\ 14.656\\ 14.651\\ 14.656\\ 14.662\\ 14.667\\ 14.673\\ 14.673\\ 14.678\\ 14.683\\ 14.689\\ 14.694\\ 14.700\\ 14.705\\ 14.714\\ 14.720\\ 14.725\\ 14.731\\ \hline \end{array}$	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 34.476 34.481 34.487 34.492 34.497 34.502 34.502 34.507 34.512 34.517 34.523 34.528 34.528 34.528 34.533 34.538 34.543	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.577 35.582 35.577 35.582 35.593 35.593 35.598 35.603 35.608 35.614 35.619 35.624 35.629	$\begin{tabular}{ c c c c c } & \Delta V \\ & -1.337 \\ & -1.319 \\ & -1.280 \\ & -1.262 \\ & -1.226 \\ & -1.175 \\ & -1.145 \\ & -1.145 \\ & -1.133 \\ & -1.131 \\ & -1.138 \\ & -1.129 \\ & -1.124 \\ & -1.140 \\ & -1.133 \\ & -1.145 \\ & -1.187 \\ & -1.229 \end{tabular}$	HJD 2457600+ 35.677 36.511 36.516 36.522 36.527 36.533 36.538 36.544 36.549 36.555 36.560 36.560 36.566 36.577 36.582 36.588 36.593 36.598
$\begin{array}{c} -1.103 \\ -1.096 \\ \hline \\ \Delta V \\ \hline \\ \hline \\ -1.088 \\ -1.084 \\ -1.110 \\ -1.139 \\ -1.180 \\ -1.207 \\ -1.243 \\ -1.267 \\ -1.304 \\ -1.325 \\ -1.341 \\ -1.368 \\ -1.368 \\ -1.369 \\ -1.394 \\ -1.404 \\ -1.410 \\ -1.408 \\ -1.415 \\ -1.406 \\ \end{array}$	$\begin{array}{c} 14.6600\\ 14.6654\\ \\\hline \\ HJD\\ 2457600+\\ \hline \\ 14.493\\ 14.497\\ 14.502\\ 14.507\\ 14.513\\ 14.513\\ 14.513\\ 14.523\\ 14.523\\ 14.528\\ 14.534\\ 14.539\\ 14.546\\ 14.552\\ 14.562\\ 14.568\\ 14.573\\ 14.579\\ 14.584\\ 14.590\\ \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{r} 34.527\\ 34.533\\ \hline \\ HJD\\ 2457600+\\ \hline \\ 14.634\\ 14.640\\ 14.645\\ 14.651\\ 14.656\\ 14.651\\ 14.656\\ 14.662\\ 14.667\\ 14.673\\ 14.673\\ 14.678\\ 14.683\\ 14.683\\ 14.694\\ 14.700\\ 14.705\\ 14.714\\ 14.720\\ 14.725\\ 14.731\\ 14.736\\ \hline \end{array}$	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 34.476 34.481 34.487 34.492 34.497 34.502 34.502 34.507 34.512 34.517 34.523 34.528 34.528 34.528 34.533 34.538 34.543 34.549	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.577 35.582 35.577 35.582 35.593 35.598 35.603 35.608 35.608 35.614 35.619 35.624 35.629 35.634	$\begin{tabular}{ c c c c c } \hline & \Delta V \\ \hline & -1.337 \\ -1.319 \\ -1.280 \\ -1.262 \\ -1.262 \\ -1.262 \\ -1.175 \\ -1.145 \\ -1.145 \\ -1.133 \\ -1.131 \\ -1.138 \\ -1.129 \\ -1.124 \\ -1.140 \\ -1.133 \\ -1.145 \\ -1.187 \\ -1.229 \\ -1.262 \end{tabular}$	HJD 2457600+ 35.677 36.511 36.516 36.522 36.527 36.533 36.538 36.544 36.549 36.555 36.560 36.566 36.571 36.577 36.582 36.588 36.593 36.598 36.604
$\begin{array}{c} -1.103 \\ -1.096 \\ \hline \\ \Delta V \\ \hline \\ \hline \\ -1.088 \\ -1.084 \\ -1.110 \\ -1.139 \\ -1.180 \\ -1.207 \\ -1.243 \\ -1.267 \\ -1.304 \\ -1.304 \\ -1.325 \\ -1.341 \\ -1.368 \\ -1.368 \\ -1.394 \\ -1.404 \\ -1.410 \\ -1.408 \\ -1.415 \\ -1.406 \\ -1.394 \\ \end{array}$	$\begin{array}{c} 14.6600\\ 14.6654\\ \\\hline \\ HJD\\ 2457600+\\ \hline \\ 14.493\\ 14.497\\ 14.502\\ 14.507\\ 14.513\\ 14.513\\ 14.513\\ 14.518\\ 14.523\\ 14.528\\ 14.534\\ 14.539\\ 14.546\\ 14.552\\ 14.562\\ 14.562\\ 14.568\\ 14.573\\ 14.579\\ 14.584\\ 14.590\\ 14.595\\ \hline \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{r} 34.527\\ 34.533\\ \hline \\ HJD\\ 2457600+\\ \hline \\ 14.634\\ 14.640\\ 14.645\\ 14.651\\ 14.656\\ 14.651\\ 14.656\\ 14.662\\ 14.667\\ 14.673\\ 14.673\\ 14.678\\ 14.683\\ 14.683\\ 14.694\\ 14.700\\ 14.705\\ 14.714\\ 14.720\\ 14.725\\ 14.731\\ 14.736\\ 14.742\\ \hline \end{array}$	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 34.476 34.481 34.487 34.492 34.497 34.502 34.502 34.507 34.512 34.517 34.523 34.528 34.528 34.528 34.533 34.538 34.549 34.554	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.577 35.582 35.577 35.582 35.578 35.593 35.598 35.603 35.603 35.608 35.614 35.619 35.624 35.629 35.634 35.640	$\begin{tabular}{ c c c c c } \hline & \Delta V \\ \hline & -1.337 \\ -1.319 \\ -1.280 \\ -1.262 \\ -1.262 \\ -1.262 \\ -1.175 \\ -1.145 \\ -1.145 \\ -1.133 \\ -1.138 \\ -1.129 \\ -1.124 \\ -1.140 \\ -1.133 \\ -1.145 \\ -1.187 \\ -1.229 \\ -1.262 \\ -1.289 \end{tabular}$	HJD 2457600+ 35.677 36.511 36.516 36.522 36.527 36.533 36.538 36.544 36.555 36.560 36.556 36.566 36.577 36.582 36.588 36.593 36.598 36.604 36.609
$\begin{array}{c} -1.103 \\ -1.096 \\ \hline \\ \Delta V \\ \hline \\ \hline \\ -1.088 \\ -1.084 \\ -1.110 \\ -1.139 \\ -1.180 \\ -1.207 \\ -1.243 \\ -1.267 \\ -1.304 \\ -1.304 \\ -1.304 \\ -1.368 \\ -1.369 \\ -1.394 \\ -1.406 \\ -1.394 \\ -1.406 \\ -1.394 \\ -1.394 \\ -1.394 \end{array}$	$\begin{array}{c} 14.6600\\ 14.6654\\ \\\hline \\ HJD\\ 2457600+\\ \hline \\ 14.493\\ 14.497\\ 14.502\\ 14.507\\ 14.513\\ 14.518\\ 14.523\\ 14.528\\ 14.528\\ 14.534\\ 14.539\\ 14.546\\ 14.552\\ 14.557\\ 14.562\\ 14.568\\ 14.573\\ 14.579\\ 14.568\\ 14.573\\ 14.579\\ 14.584\\ 14.590\\ 14.595\\ 14.601\\ \hline \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{r} 34.527\\ 34.533\\ \hline \\ HJD\\ 2457600+\\ \hline \\ 14.634\\ 14.640\\ 14.645\\ 14.651\\ 14.656\\ 14.651\\ 14.656\\ 14.662\\ 14.667\\ 14.673\\ 14.678\\ 14.683\\ 14.689\\ 14.694\\ 14.700\\ 14.705\\ 14.714\\ 14.720\\ 14.725\\ 14.714\\ 14.720\\ 14.725\\ 14.731\\ 14.736\\ 14.742\\ 14.747\\ $	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} 35.594\\ 35.599\\ \hline \\ 35.599\\ \hline \\ 2457600+\\ \hline \\ 14.781\\ 14.779\\ 14.785\\ 34.470\\ 34.476\\ 34.476\\ 34.470\\ 34.476\\ 34.481\\ 34.487\\ 34.492\\ 34.497\\ 34.502\\ 34.502\\ 34.502\\ 34.507\\ 34.512\\ 34.517\\ 34.523\\ 34.512\\ 34.517\\ 34.523\\ 34.528\\ 34.533\\ 34.538\\ 34.543\\ 34.549\\ 34.554\\ 34.559\\ 34.554\\ 34.559\\ \hline \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.577 35.582 35.577 35.582 35.578 35.598 35.603 35.603 35.608 35.614 35.619 35.624 35.629 35.634 35.640 35.645	$\begin{tabular}{ c c c c c } \hline & \Delta V \\ \hline & -1.337 \\ -1.319 \\ -1.280 \\ -1.262 \\ -1.262 \\ -1.266 \\ -1.175 \\ -1.145 \\ -1.145 \\ -1.133 \\ -1.131 \\ -1.138 \\ -1.129 \\ -1.124 \\ -1.140 \\ -1.133 \\ -1.145 \\ -1.187 \\ -1.229 \\ -1.262 \\ -1.289 \\ -1.321 \\ \end{tabular}$	HJD 2457600+ 35.677 36.511 36.516 36.522 36.527 36.533 36.538 36.544 36.549 36.555 36.560 36.566 36.571 36.577 36.582 36.588 36.593 36.598 36.604 36.609 36.615
$\begin{array}{c} -1.103 \\ -1.096 \\ \hline \\ \Delta V \\ \hline \\ \hline \\ -1.088 \\ -1.084 \\ -1.110 \\ -1.139 \\ -1.207 \\ -1.243 \\ -1.267 \\ -1.304 \\ -1.304 \\ -1.304 \\ -1.368 \\ -1.369 \\ -1.394 \\ -1.406 \\ -1.394 \\ -1.394 \\ -1.367 \\ -1.367 \\ -1.367 \\ -1.367 \\ -1.394 \\ -1.367 \\ -1.394 \\ -1.367 \\ -1.367 \\ -1.367 \\ -1.394 \\ -1.367 \\ -1.367 \\ -1.367 \\ -1.367 \\ -1.367 \\ -1.394 \\ -1.367 \\ -1.36$	$\begin{array}{c} 14.6600\\ 14.6654\\ \\\hline \\ HJD\\ 2457600+\\ \hline \\ 14.493\\ 14.497\\ 14.502\\ 14.507\\ 14.513\\ 14.518\\ 14.523\\ 14.528\\ 14.534\\ 14.534\\ 14.539\\ 14.546\\ 14.552\\ 14.557\\ 14.562\\ 14.557\\ 14.562\\ 14.568\\ 14.573\\ 14.579\\ 14.584\\ 14.590\\ 14.595\\ 14.601\\ 14.607\\ 14.60$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{r} 34.527\\ 34.533\\ \hline \\ HJD\\ 2457600+\\ \hline \\ 14.634\\ 14.640\\ 14.645\\ 14.651\\ 14.656\\ 14.651\\ 14.656\\ 14.662\\ 14.667\\ 14.673\\ 14.678\\ 14.683\\ 14.689\\ 14.694\\ 14.700\\ 14.705\\ 14.714\\ 14.720\\ 14.725\\ 14.714\\ 14.720\\ 14.725\\ 14.731\\ 14.736\\ 14.742\\ 14.747\\ 14.753\\ 14.755\\ 14.753\\ 14.753\\ 14.755\\ 14.753\\ 14.755\\ 14.753\\ 14.755\\ $	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} 35.594\\ 35.599\\ \hline \\ HJD\\ 2457600+\\ \hline \\ 14.781\\ 14.779\\ 14.785\\ 34.470\\ 34.476\\ 34.476\\ 34.470\\ 34.476\\ 34.487\\ 34.492\\ 34.497\\ 34.502\\ 34.502\\ 34.507\\ 34.512\\ 34.517\\ 34.512\\ 34.517\\ 34.523\\ 34.512\\ 34.517\\ 34.523\\ 34.528\\ 34.533\\ 34.538\\ 34.543\\ 34.549\\ 34.554\\ 34.559\\ 34.564\\ \hline \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.577 35.582 35.577 35.582 35.578 35.598 35.603 35.603 35.608 35.614 35.619 35.624 35.629 35.634 35.645 35.645 35.650	$\begin{tabular}{ c c c c c } \hline & \Delta V \\ \hline & -1.337 \\ -1.319 \\ -1.280 \\ -1.262 \\ -1.262 \\ -1.266 \\ -1.175 \\ -1.145 \\ -1.133 \\ -1.131 \\ -1.138 \\ -1.129 \\ -1.124 \\ -1.140 \\ -1.133 \\ -1.145 \\ -1.187 \\ -1.229 \\ -1.262 \\ -1.289 \\ -1.321 \\ -1.342 \\ -1.$	$\begin{array}{c} HJD\\ 2457600+\\ 35.677\\ 36.511\\ 36.516\\ 36.522\\ 36.527\\ 36.533\\ 36.538\\ 36.544\\ 36.549\\ 36.555\\ 36.560\\ 36.555\\ 36.560\\ 36.571\\ 36.582\\ 36.588\\ 36.593\\ 36.598\\ 36.598\\ 36.604\\ 36.609\\ 36.615\\ 36.620\\ 26.615\\ 36.620\\ 36.621\\ 56.620\\ 36.621\\ 56.620\\ 36.621\\ 56.620\\ 36.621\\ 56.620\\ 36.621\\ 56.620\\ 36.621\\ 56.620\\ 36.621\\ 56.620\\ 36.621\\ 56.620\\ 36.621\\ 56.620\\ 36.621\\ 56.620\\ 36.621\\ 56.620\\ $
$\begin{array}{c} -1.103 \\ -1.096 \\ \hline \\ \Delta V \\ \hline \\ \hline \\ -1.088 \\ -1.084 \\ -1.110 \\ -1.139 \\ -1.207 \\ -1.243 \\ -1.207 \\ -1.243 \\ -1.267 \\ -1.304 \\ -1.304 \\ -1.304 \\ -1.368 \\ -1.369 \\ -1.394 \\ -1.406 \\ -1.394 \\ -1.394 \\ -1.394 \\ -1.367 \\ -1.337 \\ -1.327 \\ \end{array}$	$\begin{array}{c} 14.6600\\ 14.6654\\ \\\hline \\ HJD\\ 2457600+\\ \hline \\ 14.493\\ 14.497\\ 14.502\\ 14.507\\ 14.513\\ 14.518\\ 14.523\\ 14.523\\ 14.528\\ 14.534\\ 14.539\\ 14.546\\ 14.552\\ 14.557\\ 14.562\\ 14.557\\ 14.562\\ 14.568\\ 14.573\\ 14.579\\ 14.584\\ 14.590\\ 14.595\\ 14.601\\ 14.607\\ 14.612\\ 14.612\\ 14.612\\ 14.618\\ \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{r} 34.527\\ 34.533\\ \hline \\ HJD\\ 2457600+\\ \hline \\ 14.634\\ 14.640\\ 14.645\\ 14.651\\ 14.656\\ 14.651\\ 14.656\\ 14.662\\ 14.667\\ 14.673\\ 14.678\\ 14.683\\ 14.689\\ 14.700\\ 14.705\\ 14.714\\ 14.720\\ 14.725\\ 14.714\\ 14.720\\ 14.725\\ 14.731\\ 14.736\\ 14.742\\ 14.747\\ 14.753\\ 14.753\\ 14.759\\ 14.76\\ 14.764\\ 14.764\\ 14.764\\ 14.765\\ 14.765\\ 14.755\\ 1$	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 HJD 2457600+ 14.781 14.779 14.785 34.470 34.476 34.476 34.470 34.476 34.481 34.492 34.497 34.502 34.507 34.502 34.507 34.512 34.517 34.512 34.517 34.523 34.528 34.533 34.538 34.543 34.554 34.559 34.564 34.569 34.564	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.572 35.577 35.582 35.577 35.582 35.598 35.603 35.603 35.608 35.614 35.619 35.624 35.629 35.634 35.640 35.645 35.650 35.655 25.661	$\begin{tabular}{ c c c c c } \hline & \Delta V \\ \hline & -1.337 \\ -1.319 \\ -1.280 \\ -1.262 \\ -1.262 \\ -1.266 \\ -1.175 \\ -1.145 \\ -1.133 \\ -1.131 \\ -1.138 \\ -1.129 \\ -1.124 \\ -1.140 \\ -1.133 \\ -1.145 \\ -1.187 \\ -1.229 \\ -1.262 \\ -1.289 \\ -1.321 \\ -1.342 \\ -1.358 \\ -1.$	$\begin{array}{c} HJD\\ 2457600+\\ 35.677\\ 36.511\\ 36.516\\ 36.522\\ 36.527\\ 36.533\\ 36.538\\ 36.544\\ 36.549\\ 36.555\\ 36.560\\ 36.555\\ 36.560\\ 36.571\\ 36.582\\ 36.588\\ 36.593\\ 36.598\\ 36.698\\ 36.699\\ 36.615\\ 36.620\\ 36.626\\ 26.626\\ 26.621\\ \end{array}$
$\begin{array}{c} -1.103 \\ -1.096 \\ \hline \\ & \Delta V \\ \hline \\ \hline \\ & -1.088 \\ -1.084 \\ -1.110 \\ -1.139 \\ -1.207 \\ -1.243 \\ -1.207 \\ -1.243 \\ -1.267 \\ -1.304 \\ -1.325 \\ -1.341 \\ -1.368 \\ -1.368 \\ -1.369 \\ -1.394 \\ -1.406 \\ -1.394 \\ -1.406 \\ -1.394 \\ -1.394 \\ -1.394 \\ -1.367 \\ -1.337 \\ -1.327 \\ -$	$\begin{array}{c} 14.6600\\ 14.6654\\ \\\hline \\ HJD\\ 2457600+\\ \hline \\ 14.493\\ 14.497\\ 14.502\\ 14.507\\ 14.513\\ 14.518\\ 14.523\\ 14.523\\ 14.523\\ 14.528\\ 14.534\\ 14.539\\ 14.546\\ 14.552\\ 14.557\\ 14.562\\ 14.568\\ 14.573\\ 14.579\\ 14.568\\ 14.573\\ 14.579\\ 14.584\\ 14.590\\ 14.595\\ 14.601\\ 14.607\\ 14.612\\ 14.618\\ 14.623\\ \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{r} 34.527\\ 34.533\\ \hline \\ HJD\\ 2457600+\\ \hline \\ 14.634\\ 14.640\\ 14.645\\ 14.651\\ 14.656\\ 14.651\\ 14.656\\ 14.662\\ 14.667\\ 14.673\\ 14.678\\ 14.683\\ 14.689\\ 14.689\\ 14.689\\ 14.694\\ 14.700\\ 14.705\\ 14.714\\ 14.720\\ 14.725\\ 14.714\\ 14.720\\ 14.725\\ 14.731\\ 14.736\\ 14.742\\ 14.747\\ 14.753\\ 14.759\\ 14.764\\ 14.700\\ 14.700\\ 14.705\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.764\\ 14.770\\ 14.770\\ 14.770\\ 14.764\\ 14.770\\ $	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 34.476 34.481 34.492 34.497 34.502 34.507 34.502 34.507 34.512 34.517 34.523 34.528 34.517 34.523 34.528 34.533 34.538 34.543 34.554 34.559 34.564 34.569 34.575 34.580	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.577 35.582 35.577 35.582 35.578 35.593 35.598 35.603 35.608 35.614 35.624 35.629 35.624 35.629 35.634 35.645 35.650 35.655 35.651 35.655	ΔV -1.337 -1.319 -1.280 -1.262 -1.262 -1.266 -1.175 -1.145 -1.145 -1.133 -1.131 -1.138 -1.129 -1.124 -1.140 -1.133 -1.145 -1.145 -1.145 -1.145 -1.146 -1.133 -1.129 -1.229 -1.229 -1.262 -1.229 -1.262 -1.289 -1.321 -1.383 -1.383 -1.383 -1.383 -1.383 -1.383 -1.382	$\begin{array}{c} HJD\\ 2457600+\\ \hline 35.677\\ 36.511\\ 36.516\\ 36.522\\ 36.527\\ 36.533\\ 36.538\\ 36.544\\ 36.549\\ 36.544\\ 36.549\\ 36.555\\ 36.560\\ 36.566\\ 36.571\\ 36.577\\ 36.582\\ 36.588\\ 36.593\\ 36.598\\ 36.604\\ 36.609\\ 36.615\\ 36.620\\ 36.620\\ 36.626\\ 36.631\\ 36.627\\ \end{array}$
$\begin{array}{c} -1.103 \\ -1.096 \\ \hline \\ & \Delta V \\ \hline \\ \hline \\ & -1.088 \\ -1.084 \\ -1.110 \\ -1.139 \\ -1.207 \\ -1.243 \\ -1.207 \\ -1.243 \\ -1.267 \\ -1.304 \\ -1.325 \\ -1.341 \\ -1.368 \\ -1.368 \\ -1.369 \\ -1.394 \\ -1.406 \\ -1.394 \\ -1.406 \\ -1.394 \\ -1.394 \\ -1.367 \\ -1.337 \\ -1.327 \\ -1.320 \\ -1.301 \\ \end{array}$	$\begin{array}{c} 14.6600\\ 14.6654\\ \\\hline \\ HJD\\ 2457600+\\ \hline \\ 14.493\\ 14.497\\ 14.502\\ 14.507\\ 14.513\\ 14.518\\ 14.523\\ 14.523\\ 14.523\\ 14.523\\ 14.534\\ 14.539\\ 14.546\\ 14.552\\ 14.557\\ 14.562\\ 14.568\\ 14.573\\ 14.579\\ 14.568\\ 14.573\\ 14.579\\ 14.584\\ 14.590\\ 14.595\\ 14.601\\ 14.607\\ 14.612\\ 14.618\\ 14.623\\ 14.623\\ 14.623\\ 14.623\\ 14.629\\ \hline \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} 34.527\\ 34.533\\ \\\hline\\ HJD\\ 2457600+\\ \hline\\ 14.634\\ 14.640\\ 14.645\\ 14.651\\ 14.656\\ 14.651\\ 14.656\\ 14.662\\ 14.667\\ 14.673\\ 14.678\\ 14.683\\ 14.689\\ 14.689\\ 14.689\\ 14.694\\ 14.700\\ 14.705\\ 14.714\\ 14.720\\ 14.725\\ 14.731\\ 14.736\\ 14.742\\ 14.747\\ 14.753\\ 14.759\\ 14.764\\ 14.770\\ 14.776\\ \end{array}$	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	35.594 35.599 <i>HJD</i> 2457600+ 14.781 14.779 14.785 34.470 34.476 34.476 34.476 34.481 34.492 34.497 34.502 34.507 34.502 34.507 34.512 34.517 34.523 34.528 34.528 34.533 34.538 34.543 34.554 34.559 34.564 34.559 34.564 34.575 34.580 34.585	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	36.538 36.543 <i>HJD</i> 2457600+ 34.590 34.595 35.546 35.551 35.557 35.562 35.577 35.582 35.577 35.582 35.593 35.598 35.603 35.608 35.614 35.619 35.624 35.629 35.634 35.645 35.650 35.655 35.661 35.666 35.661 35.666 35.6671	ΔV -1.337 -1.319 -1.280 -1.262 -1.226 -1.226 -1.175 -1.145 -1.145 -1.133 -1.131 -1.138 -1.129 -1.124 -1.140 -1.133 -1.145 -1.187 -1.229 -1.262 -1.289 -1.321 -1.342 -1.358 -1.383 -1.392 -1.392 -1.396	$\begin{array}{c} HJD\\ 2457600+\\ 35.677\\ 36.511\\ 36.516\\ 36.522\\ 36.527\\ 36.533\\ 36.538\\ 36.544\\ 36.549\\ 36.555\\ 36.555\\ 36.560\\ 36.566\\ 36.571\\ 36.577\\ 36.582\\ 36.588\\ 36.593\\ 36.598\\ 36.604\\ 36.609\\ 36.615\\ 36.620\\ 36.620\\ 36.621\\ 36.637\\ 36.637\\ 36.642\end{array}$

Table continued on following pages

Table 1. V1695 Aql observations, ΔB , ΔV , ΔR_c , and ΔI_c , variable star minus comparison star, cont.

ΔR_c	HJD 2457600+								
1.042	14 486	1.002	14 671	1 259	21 529	1 415	25 604	1 1 2 9	26 540
1.044	14.400	-1.095	14.071	-1.258	24.538	1 419	35.600	-1.130	26 554
-1.044	14.490	-1.089	14.070	-1.297	34.545	-1.418	35.609	-1.137	36.560
1.070	14.495	-1.090	14.082	1 265	24.552	1 432	25.620	-1.121	26 565
-1.079	14.501	-1.090	14.007	-1.303	34.555	-1.433	35.625	-1.123	36.503
1 1 4 4	14.500	-1.091	14.095	-1.381	24.559	-1.445	25.620	-1.125	26 576
-1.144	14.311	-1.100	14.096	-1.404	24.504	-1.440	25.030	-1.145	26 592
-1.100	14.510	-1.097	14.704	-1.403	24.309	-1.433	35.055	-1.143	30.382
-1.210	14.322	-1.112	14.709	-1.424	24.574	-1.433	25 646	-1.131	26 502
-1.230	14.527	-1.1//	14./10	-1.441	24.579	-1.424	25 651	-1.18/	26 509
-1.512	14.557	-1.214	14.724	-1.456	25 492	-1.427	25.656	-1.220	26 604
-1.557	14.545	-1.241	14.729	-1.230	25 400	-1.410	25.030	-1.209	30.004
-1.309	14.550	-1.270	14./35	-1.228	35.488	-1.391	35.001	-1.294	30.009
-1.5/0	14.555	-1.302	14.740	-1.184	35.494	-1.388	35.00/	-1.322	30.014
-1.5/5	14.561	-1.319	14.740	-1.158	35.499	-1.3//	35.672	-1.339	36.620
-1.401	14.500	-1.558	14./51	-1.107	35.505	-1.345	35.078	-1.30/	30.025
-1.398	14.572	-1.357	14.757	-1.080	35.510	-1.310	35.684	-1.382	36.631
-1.40/	14.5//	-1.3/4	14.763	-1.0/4	35.515	-1.292	35.690	-1.406	36.636
-1.404	14.583	-1.392	14.768	-1.069	35.520	-1.397	36.461	-1.413	36.642
-1.400	14.588	-1.404	14.774	-1.068	35.526	-1.399	36.466	-1.416	36.647
-1.396	14.594	-1.168	34.465	-1.060	35.531	-1.404	36.473	-1.425	36.653
-1.382	14.599	-1.137	34.469	-1.067	35.537	-1.418	36.478	-1.427	36.658
-1.372	14.605	-1.123	34.475	-1.079	35.542	-1.397	36.483	-1.435	36.664
-1.358	14.611	-1.137	34.480	-1.085	35.547	-1.379	36.489	-1.443	36.669
-1.338	14.616	-1.137	34.486	-1.098	35.552	-1.365	36.494	-1.432	36.675
-1.314	14.622	-1.138	34.491	-1.132	35.557	-1.351	36.500	-1.432	36.680
-1.296	14.627	-1.127	34.496	-1.170	35.563	-1.338	36.505	-1.433	36.686
-1.278	14.633	-1.140	34.501	-1.207	35.568	-1.308	36.510	-1.397	36.694
-1.248	14.638	-1.145	34.507	-1.262	35.573	-1.281	36.516	-1.384	36.700
-1.207	14.644	-1.136	34.512	-1.276	35.578	-1.259	36.521	-1.357	36.705
-1.177	14.649	-1.154	34.517	-1.315	35.583	-1.221	36.527	-1.335	36.711
-1.129	14.655	-1.188	34.522	-1.350	35.588	-1.187	36.532		
-1.103	14.660	-1.211	34.527	-1.363	35.594	-1.161	36.538		
-1.096	14.665	-1.228	34.533	-1.385	35.599	-1.150	36.543		
				1		1		1	

Table continued on next page

MAKER and fill-out of 0.25. We modeled two cool spots and one hot spot to fit the asymmetries. The hot spot vanished as the Wilson program progressed. Tycho and 2MASS photometry indicated that the spectral type fell in the G6 to G9 range so a temperature of 5500 K was chosen for the primary component with the secondary component modeling at a somewhat higher temperature. Next, the mean values from the BINARY MAKER fits a set of starting values for the wD program (Wilson and Devinney 1971; Wilson 1990, 1994, 2001, 2004; Van Hamme and Wilson 1998, 2003). This version includes Kurucz atmospheres, rather than black body, and a detailed reflection treatment along with two-dimentional limb-darkening coefficients. The differential corrections routine was iterated until convergence was achieved for a solution. The solution was computed in Mode 3, the contact binary mode. Convective parameters g = 0.32, A = 0.5were used. The light curve solution is given in Table 5.

The normalized curves overlain by our light curve solutions are shown as Figure 7a and 7b. A geometrical (Roche-lobe) representation of the system is given in Figure 8 (a, b, c, d) at light curve quadratures so that the reader may see the placement of the spots and the relative size of the stars as compared to the orbit. Table 6 gives the unspotted solution for V1695 Aql. One can compare the wD program's sum of square residual, 0.19 vs. 0.15, for the unspotted vs. the spotted model. The spotted solution presents a better numerical solution. It is noted that the unspotted solution has a somewhat smaller fill-out, 35%.

8. Conclusion

V1695 Aql is a moderate period (P = 0.4128296 day), W UMa eclipsing binary. The 17-year orbital study (more than 15,000 orbits) reveals a quadratically decreasing ephemeris. Given that the temperature for the primary component is ~5500K, from T_2 we find the secondary (smaller) star is at a hotter ~5650K. This effect is believed to be due to the actual saturated spot coverage on the primary component. The wp program solution gives a mass ratio of 0.16. Rasio (1995) stated the runaway event that results in a merger happens when the mass ratio is ~ 0.09, so we are 0.07 away from that event if this is the case. The Roche Lobe fill-out is rather large, 83% for this contact binary. This value could lead the system into an instability which could result in coalescence.

Recently, Molnar *et al.* (2017) predicted that the eclipsing binary KIC 9832227 would become a red nova in the year 2022. Table 7 shows a comparison of the parameters for KIC 9832227 with V1695 Aql to show the similarity of the two systems. Molnar (2017) has examined our period study curves and does not see the expected asymmetry (right side of the curve should

Table 1. V1695 Aql observations, ΔB , ΔV , ΔR_c , and ΔI_c , variable star minus comparison star, cont.

ΔI_c	HJD 2457600+	ΔI_c	HJD 2457600+	ΔI_c	<i>HJD</i> 2457600+	ΔI_c	HJD 2457600+	ΔI_c	<i>HJD</i> 2457600+
-1.088	14 493	-1 124	14 700	_1 408	34 580	_1 103	35 557	-1 262	36 522
-1.084	14.497	-1.118	14.705	-1.415	34.585	-1.145	35.562	-1.226	36.527
-1 110	14 502	-1.161	14 714	-1 423	34 590	-1 180	35 567	-1 175	36 533
-1.139	14.507	-1.187	14.720	-1.443	34.595	-1.231	35.572	-1.145	36.538
-1.180	14.513	-1.232	14.725	-1.451	34,599	-1.266	35.577	-1.146	36.544
-1.207	14.518	-1.269	14.731	-1.448	34.604	-1.300	35.582	-1.133	36.549
-1.243	14.523	-1.287	14.736	-1.449	34.609	-1.322	35.588	-1.131	36.555
-1.267	14.528	-1.315	14.742	-1.435	34.614	-1.347	35.593	-1.138	36.560
-1.304	14.534	-1.341	14.747	-1.431	34.618	-1.362	35.598	-1.129	36.566
-1.325	14.539	-1.352	14.753	-1.417	34.623	-1.384	35.603	-1.124	36.571
-1.341	14.546	-1.366	14.759	-1.405	34.628	-1.394	35.608	-1.140	36.577
-1.368	14.552	-1.382	14.764	-1.399	34.635	-1.413	35.614	-1.133	36.582
-1.369	14.557	-1.396	14.770	-1.354	34.641	-1.420	35.619	-1.145	36.588
-1.394	14.562	-1.402	14.776	-1.327	34.647	-1.426	35.624	-1.187	36.593
-1.404	14.568	-1.418	14.781	-1.307	34.652	-1.429	35.629	-1.229	36.598
-1.410	14.573	-1.407	14.779	-1.270	34.657	-1.428	35.634	-1.262	36.604
-1.408	14.579	-1.399	14.785	-1.252	34.662	-1.418	35.640	-1.289	36.609
-1.415	14.584	-1.130	34.470	-1.217	34.667	-1.414	35.645	-1.321	36.615
-1.406	14.590	-1.121	34.476	-1.181	34.671	-1.408	35.650	-1.342	36.620
-1.394	14.595	-1.127	34.481	-1.148	34.676	-1.399	35.655	-1.358	36.626
-1.394	14.601	-1.131	34.487	-1.328	35.463	-1.384	35.661	-1.383	36.631
-1.367	14.607	-1.136	34.492	-1.293	35.468	-1.386	35.666	-1.392	36.637
-1.337	14.612	-1.132	34.497	-1.282	35.473	-1.371	35.671	-1.396	36.642
-1.327	14.618	-1.137	34.502	-1.259	35.477	-1.337	35.677	-1.418	36.648
-1.320	14.623	-1.145	34.507	-1.244	35.482	-1.310	35.682	-1.421	36.653
-1.301	14.629	-1.136	34.512	-1.208	35.487	-1.276	35.689	-1.438	36.659
-1.284	14.634	-1.147	34.517	-1.174	35.493	-1.245	35.694	-1.438	36.664
-1.249	14.640	-1.159	34.523	-1.127	35.499	-1.404	36.462	-1.428	36.670
-1.226	14.645	-1.182	34.528	-1.087	35.504	-1.397	36.467	-1.424	36.675
-1.180	14.651	-1.224	34.533	-1.055	35.509	-1.399	36.473	-1.421	36.681
-1.141	14.656	-1.250	34.538	-1.039	35.514	-1.405	36.478	-1.415	36.686
-1.120	14.662	-1.295	34.543	-1.039	35.519	-1.397	36.484	-1.391	36.695
-1.109	14.667	-1.332	34.549	-1.037	35.525	-1.392	36.489	-1.378	36.700
-1.115	14.673	-1.353	34.554	-1.038	35.531	-1.372	36.494	-1.353	36.706
-1.106	14.678	-1.375	34.559	-1.044	35.536	-1.352	36.500	-1.318	36.711
-1.112	14.683	-1.378	34.564	-1.046	35.541	-1.330	36.505		
-1.114	14.689	-1.393	34.569	-1.057	35.546	-1.319	36.511		
-1.110	14.694	-1.408	34.575	-1.074	35.551	-1.280	36.516		

Table 2. Information on the stars used in this study.

	Star	Name	R.A. (2000) h m s	Dec. (2000) ° ' "	V	J–K	B-V
	V	V1695 Aql GSC 5149-2845 BD–03 4659	19 38 22.3027	-03 32 37.4611	10.92 ¹	0.40	0.72 ± 0.08^{1}
	С	GSC 5149-2931	19 38 23.9189	-03 35 56.9651	11.04	_	_
	K (Check)	3UC174-2249292	19 38 22.5783	-03 28 3.3563	12.25	0.30	—
¹ Høg, E., et	al. 2000.						

be steeper than that left as it is in Figure 12 of their paper, Molnar *et al.* 2017). So while the period is decreasing, it is not exponentially decaying at this time. If this phenomenon were present, it would lead to a rapid coalescence.

The extreme mass ratio binary has an inclination of 86°, which yields the rather long-duration total eclipse. The W UMa binary is of W-type (the less massive component is slightly hotter). This is unusual for deep contact binaries. Two cool spots were needed in the wp solution.

This initial study of V1695 Aql lays the groundwork for future work. More eclipse timings are needed to make a definitive study of its orbital evolution. We plan future followup observations. Of course, radial velocity curves should be obtained to determine its absolute physical character (masses in kg, radii in km, etc.).

Table 3. V1695 Aql period study.

	<i>Epoch</i> 2400000+	Cycles	Linear Residuals	Quadratic Residuals	Reference
1	51275.0350	-15409.5	-0.0366	-0.0024	Paschke 1994, 2002
2	52433.6990	-12603.0	0.0210	0.0163	Paschke 1994, 2002
3	52522.4400	-12388.0	0.0036	-0.0035	Berhard et al. 2002
4	52522.4432	-12388.0	0.0068	-0.0003	Pejcha 2005
5	52576.3098	-12257.5	-0.0008	-0.0093	Pejcha 2005
6	55405.0525	-5405.5	0.0331	-0.0014	Kazuo O-C Gateway
7	57614.6837	-53.0	-0.0064	0.0024	This Paper
8	57634.4925	-5.0	-0.0134	-0.0039	This Paper
9	57636.5626	0.0	-0.0074	0.0021	This Paper

Table 4. V1695 Aql light curve characteristics.

Filter	Phase	Magnitude Max. I	Phase	e Magnitude Max. II
	0.25		0.75	
В		-1.408 ± 0.019		-1.406 ± 0.010
V		-1.408 ± 0.016		-1.431 ± 0.005
R		-1.386 ± 0.015		-1.401 ± 0.007
I _c		-1.406 ± 0.017		-1.432 ± 0.005
Filter	Phase	Magnitude Min. II	Phase	e Magnitude Min. I
	0.0		0.5	
В		-0.993 ± 0.002		-1.077 ± 0.014
V		-1.040 ± 0.004		-1.108 ± 0.013
R		-0.993 ± 0.004		-1.078 ± 0.015
I _c		-1.040 ± 0.003		-1.108 ± 0.013
Filter		Min. I – Max. I		Min. I – Min. II
В		0.415 ± 0.021		0.084 ± 0.016
V		0.368 ± 0.020		0.068 ± 0.016
R		0.393 ± 0.019		0.085 ± 0.018
I _c		0.366 ± 0.020		0.068 ± 0.016
Filter	Max. I –	Max. II	Filter	Min. II – Max. I
В	-0.002 ±	= 0.030	В	0.331 ± 0.033
V	0.023 ±	= 0.021	V	0.300 ± 0.028
R	0.015 ±	= 0.022	R	0.308 ± 0.030
I _c	0.026 ±	= 0.022	I c	0.298 ± 0.029



Figure 6. Each night's observations in B and V are plotted to show night to night variations in observations. Blue = night 1, Green = night 2, Red = night 3, Pink = night 4.



Figure 7a. V1695 Aql B, V normalized fluxes overlaid by our solution of V1695 Aql.



Figure 7b. V1695 Aql $\rm R_{c},\, I_{c}$ normalized fluxes overlaid by our solution of V1695 Aql.





Figure 8a. V1695 Aql, geometrical representation at phase 0.00.



Figure 8c. V1695 Aql, geometrical representation at phase 0.50.

Figure 8b. V1695 Aql, geometrical representation at phase 0.25.



Figure 8d. V1695 Aql, geometrical representation at phase 0.75.

Table 5. Synthetic curve solution for V1695 Aql. Terms with errors are iterated values.

Parameter	Value
$\begin{array}{c} \lambda_{_{B}},\lambda_{_{V}},\lambda_{_{Rc}},\lambda_{_{lc}}(nm) \\ x_{_{boll,2}},y_{boll,2} \\ x_{_{11c,2lc}}I,y_{1c,2lc} \\ x_{_{11c,2lc}}I,y_{11c,2lc} \\ x_{_{1Rc,2Rc}},y_{1Rc,2Rc} \\ x_{_{1V,2V}},y_{1V,2V} \\ x_{_{1B,2B}},y_{1B,2B} \\ g_{1},g_{2} \\ A_{_{1}},A_{_{2}} \end{array}$	440, 550, 640, 790 0.649, 0.649, 0.193, 0.193 0.623, 0.623, 0.230, 0.230 0.708, 0.708, 0.229, 0.229 0.778, 0.778, 0.108, 0.108 0.847, 0.847 -0.018, -0.018 0.32 0.5
Inclination (°) T_1, T_2 (K) Ω_1, Ω_2 $q(m_2 / m_1)$ Fill-outs: $F_1 = F_2$ $L_1 / (L_1 + L_2)_{le}$	85.6 ± 0.2 $5500, 5649 \pm 3$ 2.049 ± 0.001 0.1622 ± 0.0002 $83\% \pm 1\%$ 0.805 ± 0.001 0.805 ± 0.001
$\begin{array}{c} L_{1} / (L_{1} + L_{2})_{Rc} \\ L_{1} / (L_{1} + L_{2})_{V} \\ L_{1} / (L_{1} + L_{2})_{B} \\ r_{1}, r_{2} (\text{pole}) \\ r_{1}, r_{2} (\text{side}) \\ r_{1}, r_{2} (\text{back}) \end{array}$	$\begin{array}{c} 0.803 \pm 0.002 \\ 0.800 \pm 0.001 \\ 0.792 \pm 0.001 \\ 0.525 \pm 0.002, \ 0.246 \pm 0.003 \\ 0.586 \pm 0.003, \ 0.260 \pm 0.004 \\ 0.613 \pm 0.003, \ 0.340 \pm 0.019 \end{array}$
Spot 1	Star 1
Colatitude Longitude Spot radius T–Factor	$125 \pm 180.6 \pm 0.429.5 \pm 0.10.812 \pm 0.003$
Spot 2	Star 1
Colatitude Longitude Spot radius T–Factor	$102.2 \pm 0.4 275.4 \pm 0.3 23.9 \pm 0.01 0.803 \pm 0.003$
Pshift JD ₀ (days) Period (days) $\Sigma(res)^2$	$\begin{array}{c} 0.0\\ 2457634.7038\pm 0.0003\\ 0.412755\pm 0.000006\\ 0.1468\end{array}$

Table 6. Unspotted synthetic curve solution for V1695 Aql. Terms with errors are iterated values. The values not listed are identical as those in Table 4.

Parameter	Value
Inclination (°)	87.1 ± 0.5
$T_{1}, T_{2}(K)$	$5500, 5252 \pm 4$
$\Omega_1, \overline{\Omega_2}$	2.114 ± 0.002
$q(m_2/m_1)$	0.1684 ± 0.0004
Fill–outs: $F_1 = F_2$	$34.8 \pm 0.2\%$,
$L_{1} / (L_{1} + L_{2})_{1}$	0.849 ± 0.010
$L_{1}^{1} / (L_{1}^{1} + L_{2}^{2})_{R}^{1}$	0.852 ± 0.015
$L_{1}^{1} / (L_{1}^{1} + L_{2}^{2})_{V}^{N}$	0.856 ± 0.010
$L_{1}^{1} / (L_{1}^{1} + L_{2}^{2})_{B}$	0.866 ± 0.011
r_1, r_2 (pole)	$0.509 \pm 0.002, 0.232 \pm 0.003$
r_1, r_2 (side)	$0.561 \pm 0.003, 0.243 \pm 0.003$
r_1, r_2 (back)	$0.585 \pm 0.004, 0.287 \pm 0.008$
$\Sigma(res)^2$	0.1932

Table 7. Comparison	of KIC	9832227 to	o V168:	5 Aql
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Star	q	T_{I}	T_2	Р	Ė
KIC 9832227	0.227957	5800 K	5920 K	0.4579615 d	$\begin{array}{c} 2.0 \times 10^{-6} \\ 1.7 \times 10^{-6} \end{array}$
V1685 Aql	0.1622	5500 K	5649 K	0.4128296 d	

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